IN THE CLAIMS

Please amend the claims as follows:

1. (Currently Amended) A hot-rolled austenitic iron/carbon/manganese steel sheet, the strength of which is greater than 900 MPa, the product (strength (in MPa) × elongation at fracture (in %)) of which is greater than 45 000 and the chemical composition of which comprises, the contents being expressed by weight:

 $0.5\% \le C \le 0.7\%$

 $17\% \le Mn \le 24\%$

Si ≤ 3%

 $A1 \le 0.050\%$

 $S \le 0.030\%$

 $P \le 0.080\%$

 $N \le 0.1\%$,

and, optionally, one or more elements such that:

Cr ≤ 1%

 $Mo \le 0.40\%$

Ni ≤ 1%

Cu ≤ 5%

 $Ti \le 0.50\%$

 $Nb \le 0.50\%$

 $V \le 0.50\%$,

the rest of the composition consisting of further comprising iron and inevitable impurities resulting from the smelting, the recrystallized fraction of the steel being greater than 75%, the

surface fraction of precipitated carbides of the steel being less than 1.5% and the mean grain size of the steel being less than 18 microns.

2. (Currently Amended) A hot-rolled austenitic iron/carbon/manganese steel sheet, the strength of which is greater than 900 MPa, the product (strength (in MPa) × elongation at fracture (in %)) of which is greater than 60 000 and the chemical composition of which comprises, the contents being expressed by weight:

$$0.5\% \le C \le 0.7\%$$

$$17\% \le Mn \le 24\%$$

Si ≤ 3%

 $A1 \le 0.050\%$

 $S \leq 0.030\%$

 $P \leq 0.080\%$

 $N \le 0.1\%$,

and, optionally, one or more elements such that:

Cr ≤ 1%

 $Mo \le 0.40\%$

Ni ≤ 1%

Cu ≤ 5%

 $Ti \le 0.50\%$

 $Nb \le 0.50\%$

 $V \le 0.50\%$,

the rest of the composition consisting of further comprising iron and inevitable impurities resulting from the smelting, the recrystallized fraction of the steel being equal to 100%, the

surface fraction of precipitated carbides of the steel being equal to 0% and the mean grain size of the steel being less than 10 microns.

- 3. (Currently Amended)A process for manufacturing a hot-rolled sheet made of iron/carbon/manganese steel, in which:
- <u>a semifinished product is cast from</u> a steel is smelted whose chemical composition comprises, the contents being expressed by weight:

$$0.5\% \le C \le 0.7\%$$

$$17\% \le Mn \le 24\%$$

Si ≤ 3%

 $Al \le 0.050\%$

 $S \le 0.030\%$

 $P \leq 0.080\%$

 $N \le 0.1\%$,

and, optionally, one or more elements such that:

Cr ≤ 1%

 $Mo \le 0.40\%$

Ni ≤ 1%

 $Cu \le 5\%$

 $Ti \leq 0.50\%$

 $Nb \le 0.50\%$

 $V \le 0.50\%$,

the rest of the composition consisting of further comprising iron and inevitable impurities resulting from the smelting;

- a semifinished product is cast-from this steel;
- said semifinished product of said steel composition is heated to a temperature of between 1100 and 1300°C;
- said semifinished product is rolled with an end-of-rolling temperature of 890°C or higher;
- a delay is observed between said end of rolling and a subsequent rapid cooling operation, in such a way that the point defined by said delay and said end-of-rolling temperature lies within an area defined by the ABCD'E'F'A plot, and preferably the ABCDEFA plot, of figure 1; and
 - said sheet is coiled at a temperature below 580°C.
- 4. (Original) The process as claimed in claim 3, wherein said semifinished product is cast in the form of thin strip, by being cast between steel rolls.
- 5. (Currently Amended) The manufacturing process as claimed in claim 3 or 4, wherein, after said coiling, said hot-rolled sheet is subjected to a cold deformation operation with an equivalent deformation ratio of 30% or less.
- 6. (Currently Amended) A cold-rolled austenitic iron/carbon/manganese steel sheet, the strength of which is greater than 950 MPa, the product (strength (in MPa) × elongation at fracture (in %)) of which is greater than 45000 and the chemical composition of which comprises, the contents being expressed by weight:

$$0.5\% \le C \le 0.7\%$$

$$17\% \le Mn \le 24\%$$

Si ≤ 3%

 $A1 \le 0.050\%$

 $S \le 0.030\%$

 $P \le 0.080\%$

 $N \le 0.1\%$,

and, optionally, one or more elements such that:

Cr ≤ 1%

 $Mo \le 0.40\%$

Ni ≤ 1%

Cu ≤ 5%

 $Ti \le 0.50\%$

 $Nb \le 0.50\%$

 $V \le 0.50\%$,

the rest of the composition consisting of further comprising iron and inevitable impurities resulting from the smelting, the recrystallized fraction of the structure of the steel being greater than 75%, the surface fraction of precipitated carbides of the steel being less than 1.5% and the mean grain size of the steel being less than 6 microns.

- 7. (Currently Amended) A process for manufacturing a cold-rolled austenitic iron/carbon/manganese steel sheet, wherein:
- a hot-rolled sheet obtained by the process as claimed in claim 3 or 4 is

supplied;

<u>subjected to</u> at least one cold-rolling step followed by an annealing operation is carried out, each step consisting in cold-rolling comprising:

cold-rolling said sheet and

- carrying out an annealing operation at a temperature of between 600 and 900°C for a time of between 10 and 500 seconds, followed by a cooling operation, the cooling rate being greater than 0.5°C/s,
- the austenitic grain size, before the final cold-rolling step followed by an annealing operation, being less than 18 microns.
- 8. (Original) The process for manufacturing a cold-rolled sheet as claimed in claim 7, wherein, after the final annealing, a cold-deformation operation is carried out with an equivalent deformation ratio of 30% or less.
- 9. (Currently Amended) The use of a sheet as claimed in any one of claims 1, 2 and 6 for the manufacture of A reinforcing elements that are statically or dynamically stressed , comprising the sheet of Claim 1.
- 10. (Cancelled)
- 11. (New) A reinforcing element, comprising the sheet of Claim 2.
- 12. (New) A reinforcing element, comprising the sheet of Claim 6.
- 13. (New) A process as claimed in Claim 3, in which:

a delay is observed between said end of rolling and a subsequent rapid cooling operation, in such a way that the point defined by said delay and said end-of-rolling temperature lies within an area defined by the ABCDEFA plot of figure 1.